

Chapitre 2 : des liquides Newtoniens vers les liquides viscoélastiques

1) Les liquides Newtoniens

$$\tau = \eta \dot{\epsilon} \quad \eta = \text{viscosité}$$

Pa.s

$$\epsilon = \frac{\partial u}{\partial x} \quad \text{et} \quad \dot{\epsilon} = \frac{\partial v}{\partial x}$$

u = déplacement

v = vitesse

gradient de
déplacement

gradient de
vitesse

$$\dot{\epsilon} = \frac{1}{2} \begin{bmatrix} 2 \frac{\partial v_x}{\partial x} & \frac{\partial v_y}{\partial x} + \frac{\partial v_x}{\partial y} & \frac{\partial v_z}{\partial x} + \frac{\partial v_x}{\partial z} \\ \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} & 2 \frac{\partial v_y}{\partial y} & \frac{\partial v_z}{\partial y} + \frac{\partial v_y}{\partial z} \\ - & - & 2 - \end{bmatrix}$$

tenseur des taux de
déformations

$$\tau = \eta \dot{\epsilon}$$

$$P_\eta = \eta \dot{\epsilon}^2$$

puissance dissipée

$$E_\eta = \eta \epsilon \dot{\epsilon}$$

énergie dissipée

Navier - Stokes

$$\underbrace{\rho \frac{D\vec{v}}{Dt}}_{\text{inertie}} = \rho \vec{g} - \vec{\nabla} P + \eta \vec{\Delta} \vec{v}$$

$\int dx \int dy$

$\rho_0 d\vec{x} d\vec{y} d\vec{z} \vec{g}$
 $\hookrightarrow \rho \vec{g}$

Diagram illustrating the joint probability distribution $P(x, y)$ for two discrete random variables X and Y . The horizontal axis represents X with values x and $x+dx$. The vertical axis represents Y with values y and $y+dy$. The joint probability is shown as a rectangle with width dx and height dy , labeled $P(x, y)$ below it. The marginal probabilities are indicated by the labels $P(x)$ and $P(y)$ on the axes.

$$\begin{aligned}
 & \left(P(x) dy dz - P(x+dx) dy dz \right) \vec{e}_x \\
 & + \left(P(y) dx dz - P(y+dy) dx dz \right) \vec{e}_y \\
 & = - \frac{\partial P}{\partial x} dx dy dz \vec{e}_x \\
 & \quad - \frac{\partial P}{\partial y} dx dy dz \vec{e}_y \\
 & \quad \hookrightarrow - \vec{\nabla} P
 \end{aligned}$$

$\sigma(y+dy)$
 $\sigma(y)$
 $\vec{G}(x, y, z)$

$$\begin{aligned} & - \sigma(y) dx dz + \sigma(y+dy) dx dz \\ &= \frac{\partial \sigma}{\partial y} dy dx dz \\ \hookrightarrow \frac{\partial \sigma}{\partial y} &= \left| \frac{\partial^2 \sigma_x}{\partial y^2} \right| \end{aligned}$$

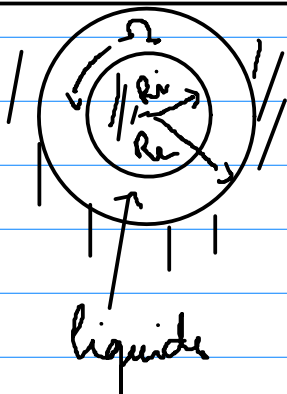
$$\vec{\Delta} \vec{v} = \left(\frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_x}{\partial z^2} \right) \vec{e}_x$$

$$+ \left(\frac{\partial^2 v_y}{\partial x^2} + \frac{\partial^2 v_y}{\partial y^2} + \frac{\partial^2 v_y}{\partial z^2} \right) \vec{e}_y$$

$$+ \left(\frac{\partial^2 v_z}{\partial x^2} + \frac{\partial^2 v_z}{\partial y^2} + \frac{\partial^2 v_z}{\partial z^2} \right) \vec{e}_z$$

2 - mesure de la viscosité

Rheomètre de Couette



Calcul du champ de vitesse

$$* \vec{v}(r, \theta, z) = v(r) \vec{u}_\theta$$

$$* 0 = \rho \vec{g} - \vec{\nabla} p + \eta \vec{\Delta} \vec{v}$$

$$\eta \frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial r v_\theta}{\partial r} \right) = 0$$

$$\frac{1}{r} \frac{\partial r v_\theta}{\partial r} = A$$

$$r v_\theta = A \frac{r^2}{2} + B$$

$$v_\theta(r) = A \frac{r}{2} + \frac{B}{r}$$

conditions aux limites

$$\varphi_{\theta}(R_e) = 0 = A \frac{R_e}{2} + \frac{B}{R_e}$$

$$\varphi_{\theta}(R_i) = \Omega R_i = A \frac{R_i}{2} + \frac{B}{R_i}$$

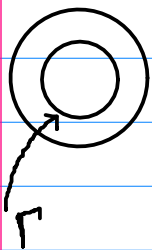
$$B = -A \frac{R_e^2}{2}$$

$$\Omega R_i = \frac{A R_i}{2} - A \frac{R_e^2}{2 R_i}$$

$$A = \frac{2 \Omega R_i^2}{R_i^2 - R_e^2}$$

$$B = -\frac{\Omega R_i^2 R_e^2}{R_i^2 - R_e^2}$$

$$\varphi_{\theta} = -\frac{\Omega R_i^2}{R_e^2 - R_i^2} r + \frac{\Omega R_i^2 R_e^2}{R_e^2 - R_i^2} \frac{1}{r}$$



$$\Gamma = -2\pi R_i H \varphi_{r\theta}(R_i) \times R_i$$

$$\varphi_{r\theta} = \eta \left(\frac{\partial \varphi_{\theta}}{\partial r} - \frac{\varphi_{\theta}}{r} \right)$$

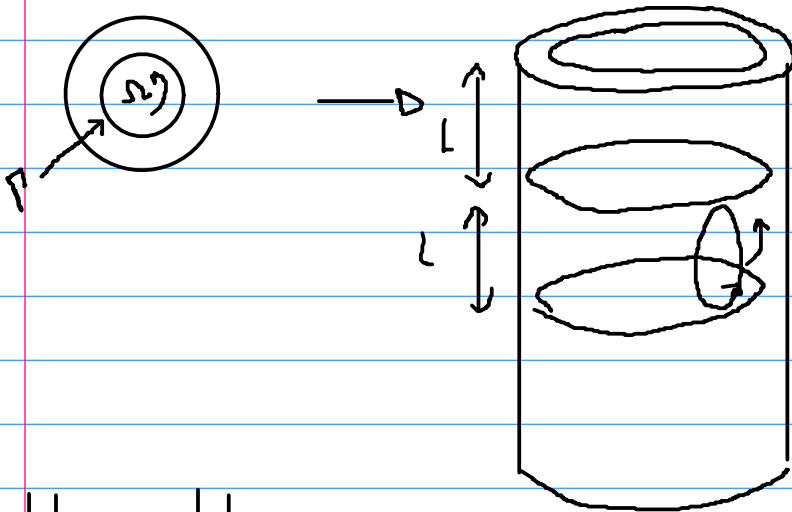
$$= -\eta \frac{\Omega R_i^2}{R_e^2 - R_i^2} - \eta \frac{\Omega R_i^2 R_e^2}{R_e^2 - R_i^2} \frac{1}{r^2}$$

$$+\eta \frac{\Omega R_i^2}{R_e^2 - R_i^2} - \eta \frac{\Omega R_i^2 R_e^2}{R_e^2 - R_i^2} \frac{1}{r^2}$$

$$\varphi_{r\theta}(R_i) = -\eta \frac{\Omega R_e^2}{R_e^2 - R_i^2}$$

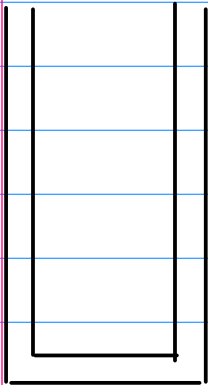
$$\Gamma = 2\pi R_i^2 H \eta \frac{\Omega R_e^2}{R_e^4 - R_i^4} = \eta \times 2\pi H \frac{\Omega R_i^2 R_e^2}{R_e^2 - R_i^2} \propto \eta \underbrace{\hspace{2cm}}_{\text{facteur géométrique}}$$

Remarque $R_e \sim R_i \Rightarrow$ grands couples



$\rightarrow$ symétrie par translation en z ?

$\exists$ instabilité à grande vitesse



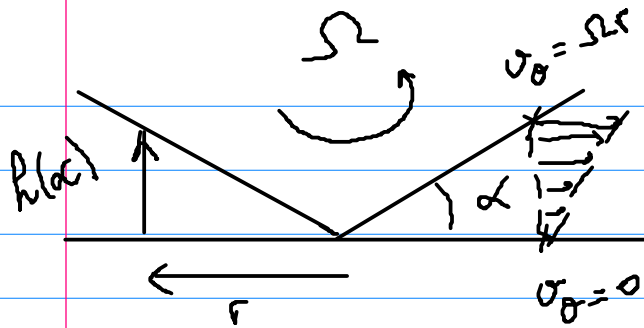
} liquide cisailé $\Rightarrow$ couple additionnel

Solution



$$1 - \dot{\epsilon} = -2\Omega \frac{R_e^2}{R_e^2 - R_i^2}$$

$$2 - \dot{\epsilon} ?$$



$$h(\alpha) = \frac{h}{r} \sim \alpha$$

$$\dot{\epsilon} \sim \frac{\partial v_\theta}{\partial r} \sim \frac{v_\theta}{h} = \frac{\Omega r}{h}$$

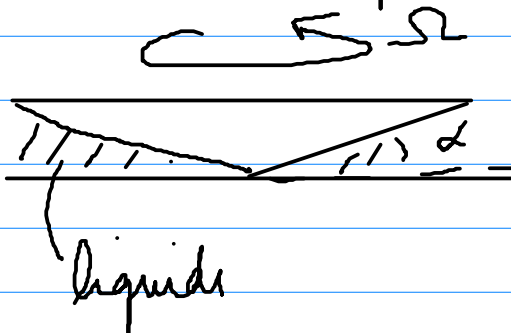
$$\dot{\epsilon} = \frac{\Omega}{\alpha}$$

$\Rightarrow \dot{\epsilon}$ indépendant de r

$\Rightarrow$ cisaillement homogène dans le cône

① $\dot{\epsilon} = \dot{\epsilon}$ autour du cylindre en fixant Ω

Rhéomètre cône-plan



$\dot{\epsilon}$ homogène
 Ω fixe
 même r nécessaire
 pour faire tourner le cône

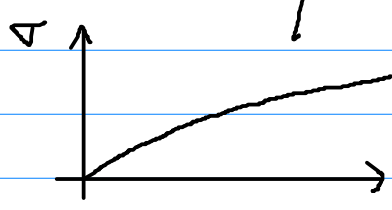
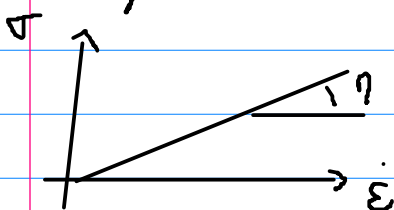
$$\Omega \Rightarrow \eta$$

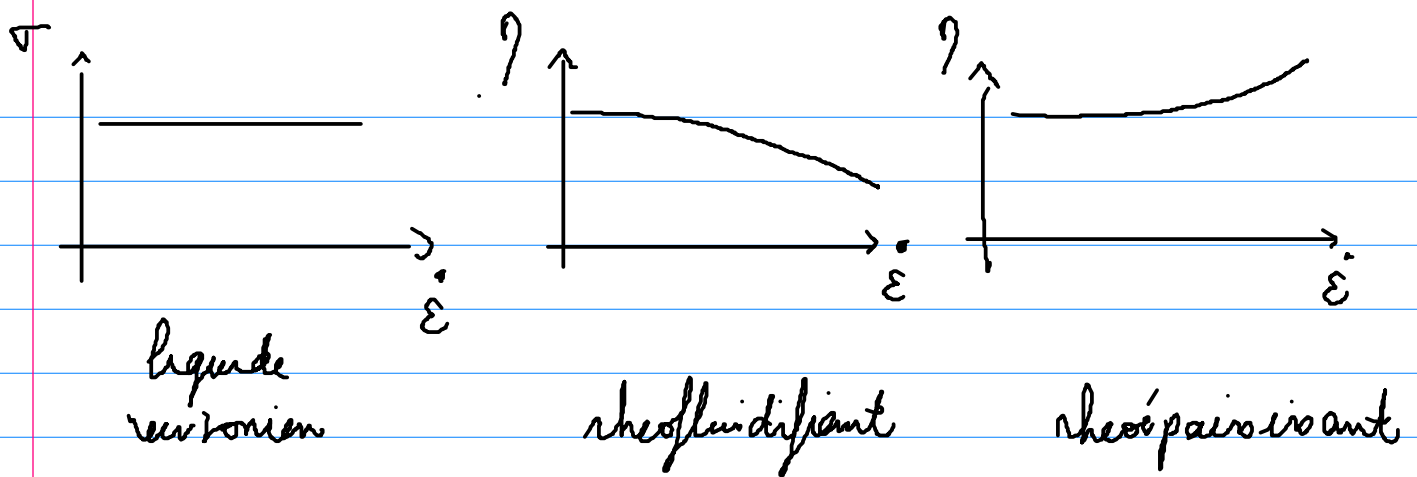
2. Les liquides non Newtoniens

liquide newtonien

$$\tau = \eta \dot{\epsilon}$$

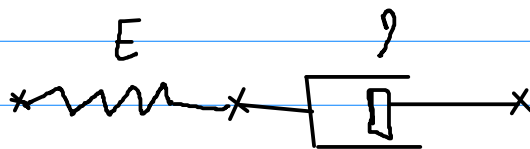
avec η cst





3 - Les liquides viscoélastiques

a) Le modèle de Maxwell



$$\dot{\sigma} + \frac{E}{\eta} \sigma = E \dot{\epsilon}$$

$$\tau = \frac{\eta}{E}$$

b) Temps caractéristique et nombre de Deborah

$$\tau = \frac{\eta}{E} \quad \longleftrightarrow \quad \tau_s \text{ temps de sollicitation}$$

$$De = \frac{\tau}{\tau_s}$$

Nombre de Deborah

$De \gg 1$
 → ms élastique
 $De \ll 1$
 → visqueuse

eau $\eta \approx 10^{-3} \text{ Pa.s}$ $\tau \approx 10^{-12} \text{ s}$
 $E \approx 10^9 \text{ Pa}$

huiles silicones $\eta \approx 2500 \text{ Pa.s}$ $\tau \approx 0,5 \text{ s}$
 $E \approx 5000 \text{ Pa}$

Glace $\eta \sim 10^{13} \text{ Pa}\cdot\text{s}$ $\tau \sim 10^4 \text{ s}$
 $E \sim 10^9 \text{ Pa}$

Petres - Mineraux $\eta = 10^{21} \text{ Pa}\cdot\text{s}$ $\tau \sim 10^{11} \text{ s}$
 $E = 10^{11} \text{ Pa}$

c) mesure de viscoélasticité - Rhéologie

liquide Newtonien $\sigma = \eta \dot{\epsilon}$
 liquide $\left\{ \begin{array}{l} \text{complexe} \\ \text{viscoélastique} \end{array} \right.$ $\sigma^* = \eta^* \dot{\epsilon}^*$

$$\eta^* = \eta - i \frac{E}{\omega}$$

$$\epsilon^* = \epsilon_0 e^{i\omega t}$$

$$\sigma^* = \left(\eta - i \frac{E}{\omega} \right) \epsilon_0 e^{i\omega t} \times i\omega$$

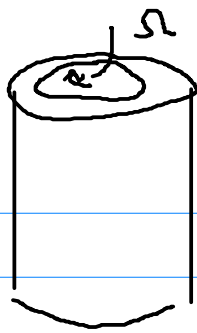
$$= (E + i\omega\eta) \epsilon_0 e^{i\omega t} = (G' + iG'') \epsilon^*$$

module
de stockage $\uparrow$
 module
de perte $\uparrow$

$$G' = E \quad G'' = \eta\omega$$

$$\eta^* = \eta - i \frac{E}{\omega} = \eta' - i\eta'' \quad \left\{ \begin{array}{l} \eta' = \eta \\ \eta'' = E/\omega \end{array} \right.$$

$$\sigma = \underbrace{E \epsilon_0 \cos \omega t}_{\text{en phase}} - \underbrace{\omega \eta \epsilon_0 \sin \omega t}_{\text{en opposition de phase.}}$$



$$\Gamma = 2\pi R_i^2 H \sigma$$

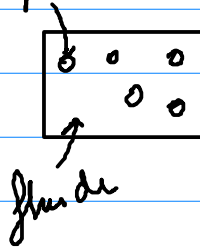
$$= \Gamma' \cos \omega t + \Gamma'' \sin \omega t$$

$$\sigma = \frac{2\epsilon^0}{R_e^2 - R_i^2} \Omega \eta$$

$$\Gamma'' = 4\pi H \frac{R_i^2 R_e^2}{R_e^2 - R_i^2} \Omega \eta'' \quad \eta'' = \frac{\epsilon}{\omega}$$

$$\Gamma' = 4\pi H \frac{R_i^2 R_e^2}{R_e^2 - R_i^2} \Omega \eta' \quad \eta' = \eta$$

grains 4. L' exemple des suspensions



$$\phi = \frac{V_{\text{grains}}}{V_{\text{total}}}$$

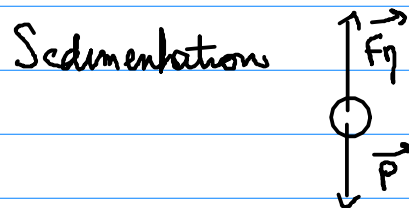
a) Le nombre de Peclet

$$Pe = \frac{\text{effets hydro}}{\text{effets de diffusion}}$$

$$= \frac{UL}{D}$$

exemple correction par sedimentation
vs diffusion

Coefficient de diffusion $D = \frac{k_B T}{6\pi\eta R}$



$$F_\eta = 6\pi\eta R U$$

$$P = \frac{4}{3}\pi R^3 \rho g$$

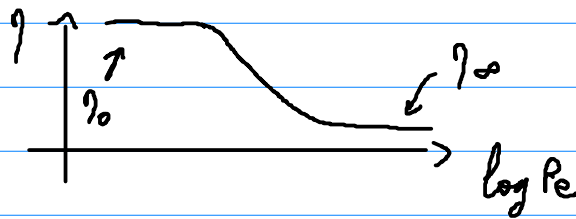
$$F_\eta = P \Rightarrow U = \frac{2}{9} \frac{\rho R^2 g}{\eta}$$

$$Pe = \frac{U \times 2R}{D} = \frac{2}{9} \frac{\rho R^2 g}{\eta} \times 2R \times \frac{6\pi\eta R}{k_B T} = \frac{8\pi \rho g R^4}{3 k_B T}$$

$$\Rightarrow Re < 1 \quad R < \left(\frac{3k_B T}{8\pi\eta g} \right)^{1/4} = 200 \text{ nm}$$

$R < 200 \text{ nm}$ $\Rightarrow$ particules browniennes
 $\Rightarrow$ suspensions stables

b) viscosité des suspensions



Re petit $\Rightarrow$ interne faible η_0
 Re grand $\Rightarrow$ gr interne η_∞

caractère rhéofluidifiant
 = alignement des
 particules $\propto$ grande
 interne.

c) Evolution de la viscosité avec ϕ

loi d'Einstein

ϕ petit $\Rightarrow$ comportement linéaire

$$\eta = \eta_s (1 + 2,5\phi)$$

Modèle d'Einstein

Solution = suspension $\tilde{a} \phi$

$\hookrightarrow$ suspension $\tilde{a} \phi + d\phi$ $\downarrow$ Einstein

$$\eta(\phi + d\phi) = \eta(\phi) (1 + 2,5 d\phi)$$

volume
exclu

$$d\eta = 2,5 \eta(\phi) d\phi$$

$$\hookrightarrow d\eta = 2,5 \eta(\phi) \frac{d\phi}{1 - K\phi}$$

$$\eta = \eta_s (1 - K\phi)^{-\frac{2,5}{K}}$$

ex : les émulsions apprivoisées

{ émulsions huile dans eau
particules suspendues = gouttes d'huile

d) Modéliser la rhéologie d'une suspension

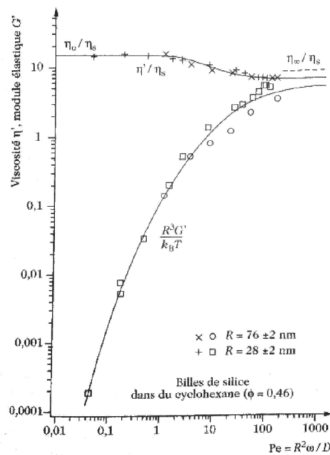
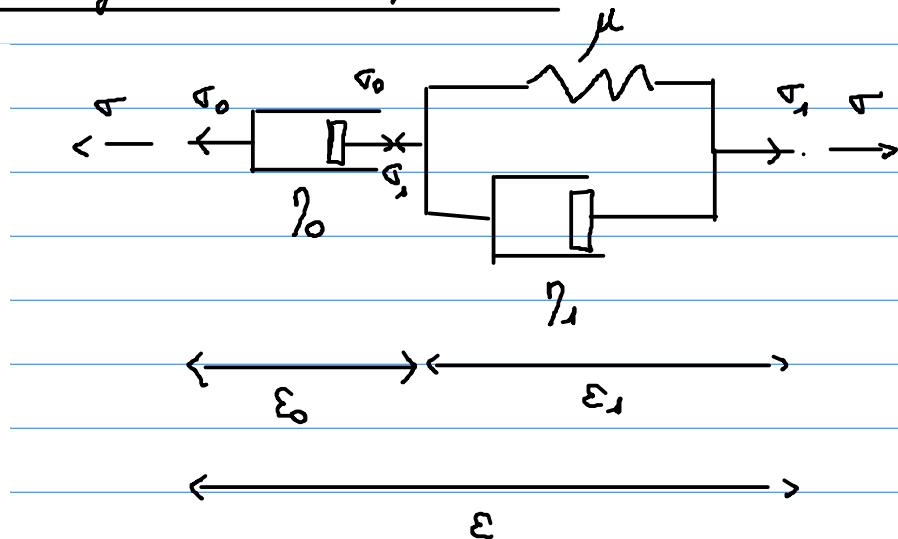


Figure 7.31. Viscosité η' et module élastique G' en fonction du nombre de Péclet [Meilena et al. 1987].



$$\varepsilon = \varepsilon_0 + \varepsilon_1$$

$$\begin{aligned} \sigma &= \eta_0 \dot{\varepsilon}_0 \\ &= \mu_1 \varepsilon_1 + \eta_1 \dot{\varepsilon}_1 \end{aligned}$$

$$\dot{\varepsilon} = \frac{\sigma}{\eta_0} + \frac{\sigma}{\eta_1} - \frac{\mu_1}{\eta_1} \varepsilon_1$$

$$= \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right) \sigma - \frac{\mu_1}{\eta_1} (\varepsilon - \varepsilon_0)$$

$$\dot{\varepsilon} = \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right) \dot{\sigma} - \frac{\mu_1}{\eta_1} \left(\dot{\varepsilon} - \frac{\dot{\sigma}}{\eta_0} \right)$$

$$\varepsilon = \varepsilon_0 \cos \omega t$$

$$\varepsilon^* = \varepsilon_0 e^{i\omega t}$$

$$\sigma^* = \sigma_0 e^{i\omega t}$$

$$-\omega^2 \varepsilon^* = \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right) i\omega \sigma^* - \frac{\mu_1}{\eta_1} \left(i\omega \varepsilon^* - \frac{\sigma^*}{\eta_0} \right)$$

$$\left(-\omega^2 + \frac{\mu_1}{\eta_1} i\omega \right) \varepsilon^* = \left(\left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right) i\omega + \frac{\mu_1}{\eta_0 \eta_1} \right) \sigma^*$$

$$\mathcal{V}^* = \frac{-\omega^2 + i\omega \frac{\mu_1}{\eta_1}}{\left(\frac{1}{\eta_0} + \frac{1}{\eta_1}\right)i\omega + \frac{\mu_1}{\eta_0\eta_1}} \varepsilon^*$$

$$= \frac{(-\omega^2 + i\omega \frac{\mu_1}{\eta_1}) \left(\frac{\mu_1}{\eta_0\eta_1} - i\omega \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right) \right)}{\left(\frac{\mu_1}{\eta_0\eta_1} \right)^2 + \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right)^2 \omega^2} \varepsilon^*$$

$$\frac{\mathcal{V}^*}{\varepsilon^*} = \frac{-\omega^2 \cancel{\mu_1}/\eta_0\eta_1 + \omega^2 \frac{\mu_1}{\eta_1} \cancel{\left(\frac{1}{\eta_0} + \frac{1}{\eta_1}\right)}}{\left(\frac{\mu_1}{\eta_0\eta_1} \right)^2 + \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right)^2 \omega^2} + i\omega \frac{\frac{\mu_1^2}{\eta_0\eta_1} + \omega^2 \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right)}{\left(\frac{\mu_1}{\eta_0\eta_1} \right)^2 + \left(\frac{1}{\eta_0} + \frac{1}{\eta_1} \right)^2 \omega^2}$$

$$= \underbrace{\frac{\mu_1 \omega^2 \eta_0^2}{\mu_1^2 + (\eta_1 + \eta_0)^2 \omega^2}}_{G'} + i\omega \eta_0 \underbrace{\frac{\mu_1^2 + \eta_1(\eta_0 + \eta_1) \omega^2}{\mu_1^2 + (\eta_1 + \eta_0)^2 \omega^2}}_{G'' = \eta \omega}$$

$$\eta_\infty = \frac{\eta_1 \eta_0}{\eta_1 + \eta_0}$$

$$\tau_0 = \frac{\eta_1}{\mu_1}$$

$$\tau_1 = \frac{\eta_1 + \eta_0}{\mu_1}$$

$$\tau_2 = \frac{\eta_0}{\mu_1}$$

$$G' = \frac{\eta_0^2 \mu_1 \omega^2}{\mu_1^2 + (\eta_1 + \eta_0)^2 \omega^2} = \frac{\mu_1 \omega^2}{\frac{1}{\tau_2^2} + \left(\frac{\eta_1}{\eta_\infty} \right)^2 \omega^2}$$

$$\frac{\eta_1}{\eta_\infty} = \frac{\eta_1 + \eta_0}{\eta_0}$$

$$\xrightarrow{\omega \rightarrow 0} G' \rightarrow 0 \quad G' \sim \tau_2^2 \mu_1 \omega^2$$

$$\xrightarrow{\omega \rightarrow +\infty} \left(\frac{\eta_\infty}{\eta_1} \right)^2 \mu_1$$

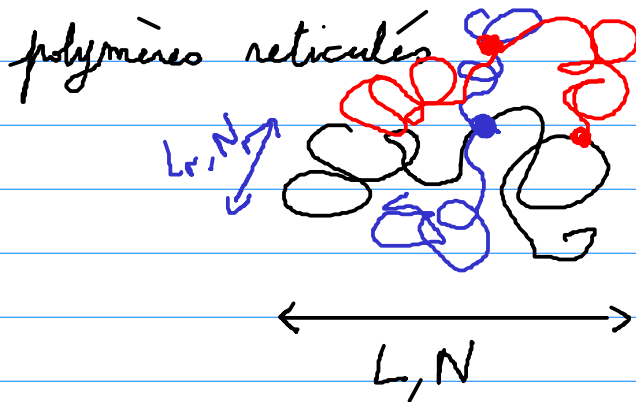
$$\eta(\omega) = \eta_0 \frac{\mu_1^2 + \eta_1 (\eta_1 + \eta_0) \omega^2}{\mu_1^2 + (\eta_1 + \eta_0)^2 \omega^2}$$

$$= \eta_0 \frac{1 + 2\tau_0 \tau_1 \omega^2}{1 + \tau_1^2 \omega^2}$$

$$\xrightarrow{\omega \rightarrow 0} \eta_0$$

$$\xrightarrow{\omega \rightarrow +\infty} \eta_\infty = \frac{\eta_1 \eta_0}{\eta_1 + \eta_0}$$

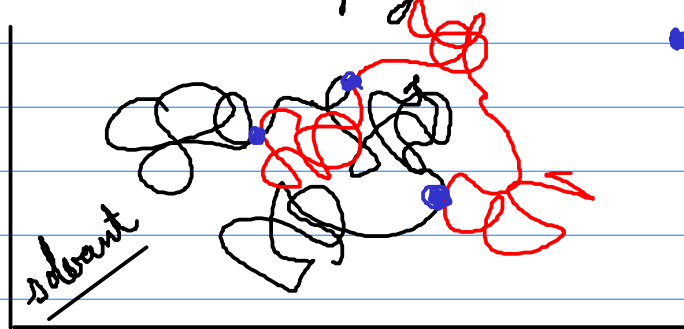
5) L'exemple des solutions de polymères



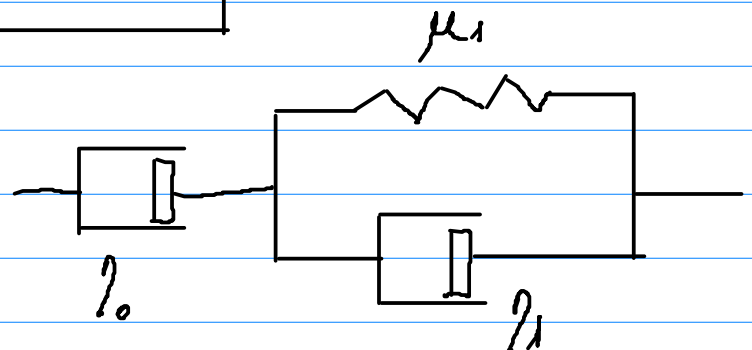
$$L = \sqrt{N} a$$

$$L_r = \sqrt{N_r} a$$

ici = solution de polymère



un modèle mécanique



$$G' = \mu_1 \frac{\eta_0^2 \omega^2}{\mu_1^2 + (\eta_0 + \eta_1)^2 \omega^2}$$

$\omega \rightarrow 0 \rightarrow \frac{\eta_0^2}{\mu_1} \omega^2$
 $\omega \rightarrow +\infty \rightarrow \mu_1 \frac{\eta_0^2}{(\eta_0 + \eta_1)^2}$

$$G'' = \eta_0 \omega \frac{\mu_1^2 + \eta_1 (\eta_0 + \eta_1) \omega^2}{\mu_1^2 + (\eta_0 + \eta_1)^2 \omega^2}$$

$\omega \rightarrow 0 \rightarrow \eta_0 \omega$
 $\omega \rightarrow +\infty \rightarrow \frac{\eta_0 \eta_1}{\eta_0 + \eta_1} \omega$

