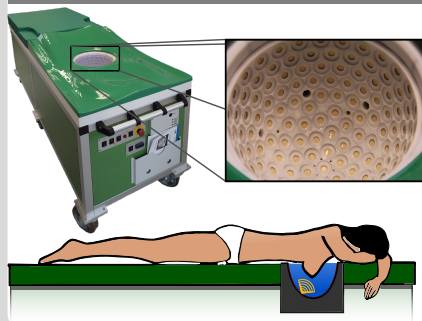


Analysis and optimization of ray-based 3D Ultrasound Tomography

Workshop ARPE

Pierre-Antoine Comby | September 17, 2020

INSTITUT FOR DATA PROCESSING AND ELECTRONICS



Groundwork

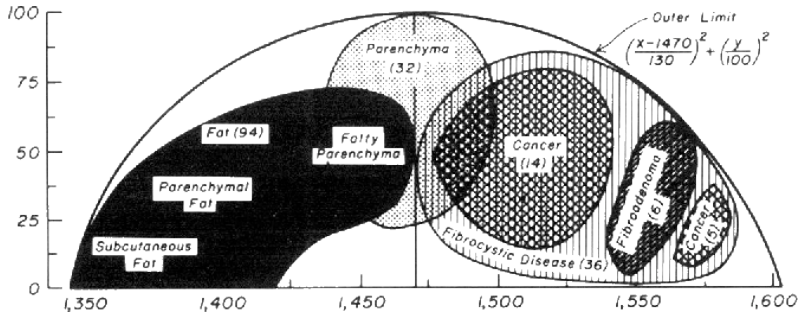


Figure 1: Acoustic characteristic of breast tissues: Attenuation/Velocity

Ultrasonic Computed Tomography

Groundwork

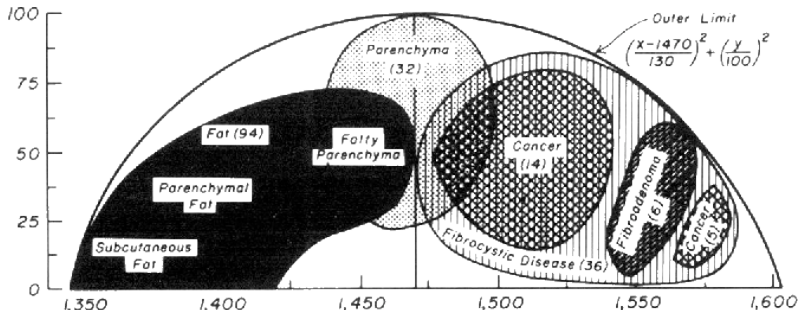


Figure 1: Acoustic characteristic of breast tissues: Attenuation/Velocity

Ultrasonic Computed Tomography

- 3D (world premiere)
- High resolution (tumour <5mm)
- Multi-modal imaging

Groundwork

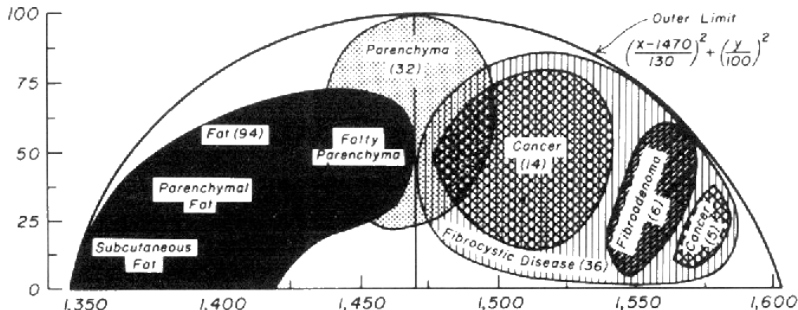
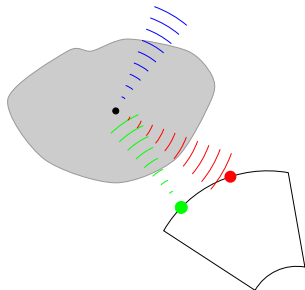


Figure 1: Acoustic characteristic of breast tissues: Attenuation/Velocity

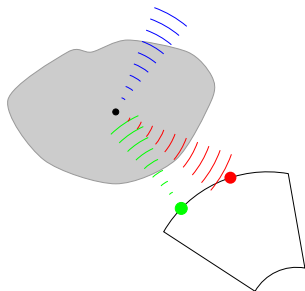
Ultrasonic Computed Tomography

- 3D (world premiere)
- High resolution (tumour <5mm)
- Multi-modal imaging
- no uses of X-rays
- Cost effective

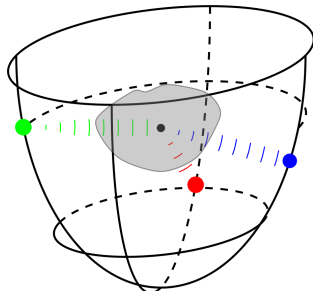
Device Principle



(a) 2D



(a) 2D



(b) 3D

Figure 2: 2D vs 3D Tomography

Device Principle

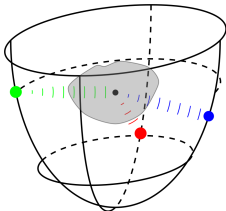


Figure 3: 3D Tomography

- Acoustics measurements
 - **Speed of sound**
 - Attenuation
 - Reflectivity

Device Principle

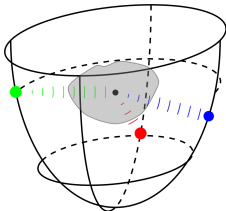
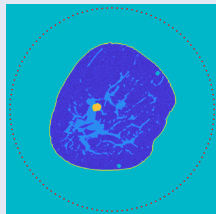


Figure 3: 3D Tomography

- Acoustics measurements
 - **Speed of sound**
 - Attenuation
 - Reflectivity

Simulation Framework

- 2D High Res. acquisition simulation
 - Groundtruth: 1px = 0.1 mm



Device Principle

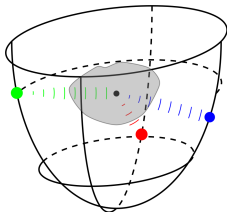


Figure 3: 3D Tomography

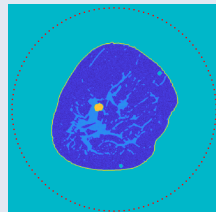
■ Acoustics measurements

- **Speed of sound**
- Attenuation
- Reflectivity

Simulation Framework

■ 2D High Res. acquisition simulation

- Groundtruth: 1px = 0.1 mm
- Based on segmented coronal MRI image



Device Principle

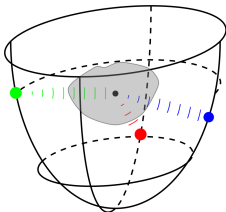


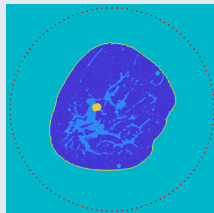
Figure 3: 3D Tomography

■ Acoustics measurements

- **Speed of sound**
- Attenuation
- Reflectivity

Simulation Framework

- 2D High Res. acquisition simulation
 - Groundtruth: 1px = 0.1 mm
 - Based on segmented coronal MRI image
- Compress Pulse $f=2.5\text{MHz}$



Device Principle

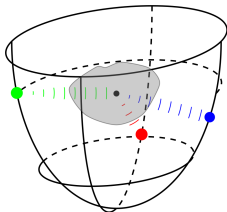


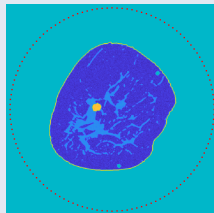
Figure 3: 3D Tomography

■ Acoustics measurements

- **Speed of sound**
- Attenuation
- Reflectivity

Simulation Framework

- 2D High Res. acquisition simulation
 - Groundtruth: 1px = 0.1 mm
 - Based on segmented coronal MRI image
- Compress Pulse $f=2.5\text{MHz}$
 - $\nearrow f \implies \searrow \text{px size}$



Device Principle

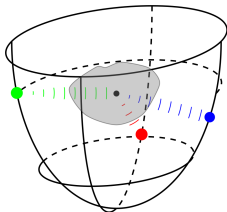


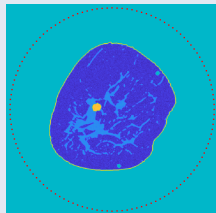
Figure 3: 3D Tomography

■ Acoustics measurements

- **Speed of sound**
- Attenuation
- Reflectivity

Simulation Framework

- 2D High Res. acquisition simulation
 - Groundtruth: 1px = 0.1 mm
 - Based on segmented coronal MRI image
- Compress Pulse $f=2.5\text{MHz}$
 - $\nearrow f \implies \searrow$ px size
 - $\searrow f \implies \nearrow$ SNR and depth of field



Physics and Modelling

Transmission and Reflection Tomography

Speed of sound tomography

$$c = \frac{\Delta L}{\Delta t} \longrightarrow t = \int \frac{1}{c} dl$$

- Transmission tomography
- *a priori* for Reflexion tomography

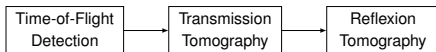
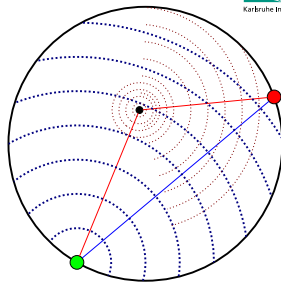
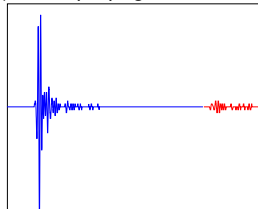


Figure 4: Reconstruction steps for USCT



(a) Wave propagation in USCT.



(b) A-Scan acquisition at Receiver.

Figure 5: Data acquisition in 2D

Base equations

- Wave Equation (Fourier Space, $k = \omega/c(\mathbf{x})$)

$$\nabla^2 P(\mathbf{x}, \omega) + k^2 P(\mathbf{x}, \omega) = 0$$

Base equations

- Wave Equation (Fourier Space, $k = \omega/c(\mathbf{x})$)

$$\nabla^2 P(\mathbf{x}, \omega) + k^2 P(\mathbf{x}, \omega) = 0$$

- Assuming an infinite frequency: A *ray* between an emitter and a receiver verifies the *Eikonal Equation*

$$\frac{d}{dl} = \left(\frac{1}{c} \frac{d\mathbf{x}}{dl} \right) = \nabla \left(\frac{1}{c} \right)$$

$$t = \int_{\mathcal{R}} \frac{1}{c} dl$$

Base equations

- Wave Equation (Fourier Space, $k = \omega/c(\mathbf{x})$)

$$\nabla^2 P(\mathbf{x}, \omega) + k^2 P(\mathbf{x}, \omega) = 0$$

- Assuming an infinite frequency: A *ray* between an emitter and a receiver verifies the *Eikonal Equation*

$$\frac{d}{dl} = \left(\frac{1}{c} \frac{d\mathbf{x}}{dl} \right) = \nabla \left(\frac{1}{c} \right)$$

$$t = \int_{\mathcal{R}} \frac{1}{c} dl$$

Base equations

- Wave Equation (Fourier Space, $k = \omega/c(\mathbf{x})$)

$$\nabla^2 P(\mathbf{x}, \omega) + k^2 P(\mathbf{x}, \omega) = 0$$

- Assuming an infinite frequency: A ray between an emitter and a receiver verifies the *Eikonal Equation*

$$\frac{d}{dl} = \left(\frac{1}{c} \frac{d\mathbf{x}}{dl} \right) = \nabla \left(\frac{1}{c} \right)$$

$$t = \int_{\mathcal{R}} \frac{1}{c} dl$$

- A ray is the fastest path between an Emitter and a Receiver.

Base equations

- Wave Equation (Fourier Space, $k = \omega/c(\mathbf{x})$)

$$\nabla^2 P(\mathbf{x}, \omega) + k^2 P(\mathbf{x}, \omega) = 0$$

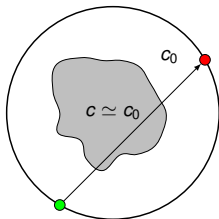
- Assuming an infinite frequency: A ray between an emitter and a receiver verifies the *Eikonal Equation*

$$\frac{d}{dl} = \left(\frac{1}{c} \frac{d\mathbf{x}}{dl} \right) = \nabla \left(\frac{1}{c} \right)$$

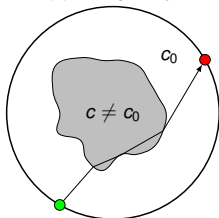
$$t = \int_{\mathcal{R}} \frac{1}{c} dl$$

- A ray is the fastest path between an Emitter and a Receiver.
- ray path \mathcal{R} and speed of sound unknown.

Infinite frequency rays



(a) Straight rays



(b) Bent rays

Straight Rays

- Homogeneous medium
- shortest path = fastest path
- Bresenham Line's Algorithm

Bent Rays

- Heterogeneous medium
- shortest path \neq fastest path
- Use Fast Marching Map (FMM) to compute the path

Figure 6: Simple rays approximations

- Differential Approach

$$\delta t = \int_{\mathcal{R}} (s(\mathbf{x}) - s_0) dl = \int_{\mathcal{R}} \frac{1}{c(\mathbf{x})} - \frac{1}{c_0} dl$$

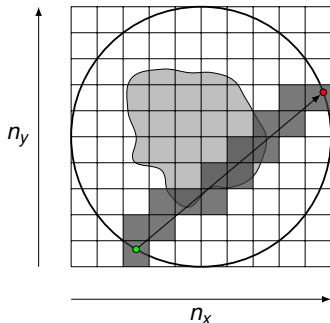
- Discrete space, for the k -th ray:

$$\delta t_k = \sum_{i=1}^{n_k} l_{ki} \delta s_i$$

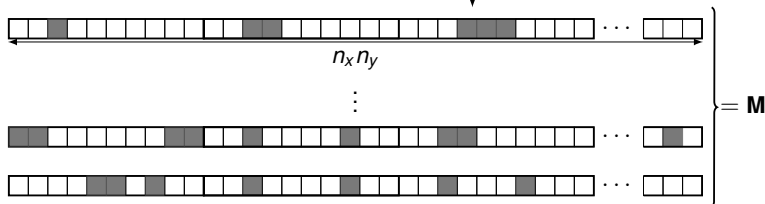
- matrix formalism:

$$\underbrace{\begin{bmatrix} \delta t_1 \\ \delta t_2 \\ \vdots \\ \delta t_m \end{bmatrix}}_{\mathbf{y}} = \underbrace{\begin{bmatrix} l_{11} & l_{12} & \cdots & l_{1n} \\ l_{21} & l_{22} & \cdots & l_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ l_{m1} & l_{m2} & \cdots & l_{mn} \end{bmatrix}}_{\mathbf{M}} \cdot \underbrace{\begin{bmatrix} \delta s_1 \\ \delta s_2 \\ \vdots \\ \delta s_n \end{bmatrix}}_{\delta \mathbf{s}} \longrightarrow \delta \mathbf{y} = \underbrace{\mathbf{M} \mathcal{I}(\mathbf{c})}_{\mathcal{M}}$$

Matrix construction



by construction, M is sparse.
(99% of coefficient are zeros in 2D)



Drawbacks of infinite frequency tomography

- Important sparsity
- High sensibility to noise
- Mathematical conception, no physical origins

Drawbacks of infinite frequency tomography

- Important sparsity
- High sensibility to noise
- Mathematical conception, no physical origins

To solve these problems, Introducing the:

Finite Frequency Tomography

- Theory stolen to geophysics and petrol prospectors
- A step towards *full-wave* approach
- Consider the complete Fresnel Zone for information

Defining the Fresnel zone

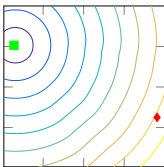
Fresnel Zone

The Fresnel is the region of space who interact constructively on the received wave

$$\delta\tau(F) = \tau(EF) + \tau(FR) - \tau(ER) \leq \frac{1}{2f}$$

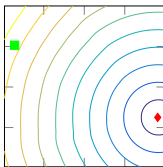
Where $\tau(EF)$, $\tau(FR)$, $\tau(ER)$, are the time of flight on the according paths.

time to emitter



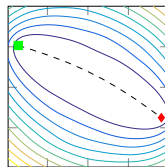
+

time to receiver



=

total travel time



Fat ray Kernel

In the Fresnel Zone we defines a
sensibility Kernel

$$\delta t_k = \int_V \delta K_{t_k}(\mathbf{x}) \delta s(\mathbf{x}) d\mathbf{x}$$

Fat ray Kernel

In the Fresnel Zone we defines a
sensibility Kernel

$$\delta t_k = \int_V \delta K_{t_k}(\mathbf{x}) \delta s(\mathbf{x}) d\mathbf{x}$$

- $K_{t_k,i} \simeq \frac{\partial t_k}{\partial c_i}$ sensitivity
- Different weights methods for fat Ray

Fat ray Kernel

In the Fresnel Zone we defines a
sensitivity Kernel

$$\delta t_k = \int_V \delta K_{t_k}(\mathbf{x}) \delta s(\mathbf{x}) d\mathbf{x}$$

- $K_{t_k,i} \simeq \frac{\partial t_k}{\partial c_i}$ sensitivity
- Different weights methods for fat Ray

Naive approach: Spread value of
bent ray /straight ray

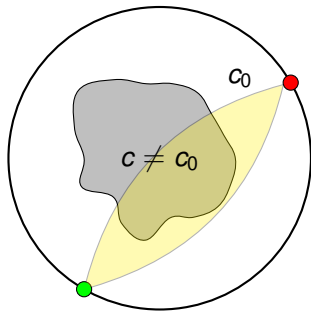


Figure 7: Fresnel Zone for Fat Ray

Fat ray Kernel

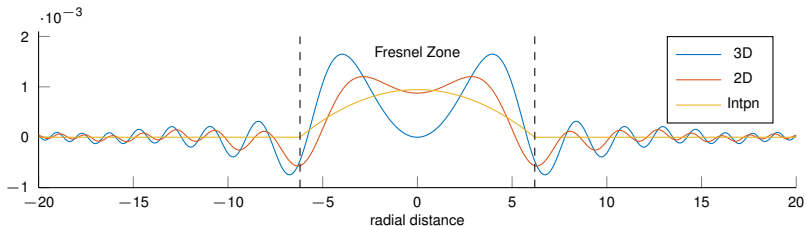


Figure 8: Comparison of Fat ray kernels

- Linear Interpolated Kernel very naive
- Fréchet Kernel (Born/Rytov Approximation)

Transducer limitations

- Opening angle (real $\simeq 30^\circ$)
- Number of ray = (Number of Transducer)²
- Geometrical Artifacts

Transducer limitations

- Opening angle (real $\simeq 30^\circ$)
- Number of ray = (Number of Transducer) 2
- Geometrical Artifacts

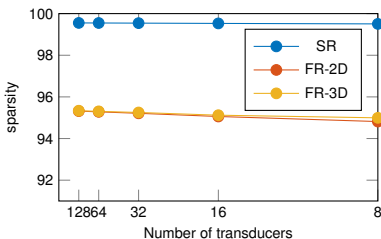
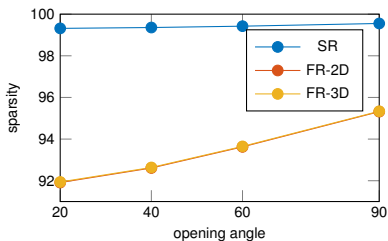


Figure 9: Sparsity of Matrix for different ray methods

Inverse Problem

- ill-posed problem $M \neq N$
- ill conditioned $\xi(\mathbf{M}) > 10^{10}$ (good value < 10)

Inverse Problem

- ill-posed problem $M \neq N$
- ill conditioned $\xi(\mathbf{M}) > 10^{10}$ (good value < 10)
- M is sparse
- M is big (memory problems)

Inverse Problem

- ill-posed problem $M \neq N$
- ill conditioned $\xi(\mathbf{M}) > 10^{10}$ (good value < 10)
- M is sparse
- M is big (memory problems)

$$\mathbf{y} = \mathbf{M}\mathbf{x}$$

Inverse Problem

- ill-posed problem $M \neq N$
- ill conditioned $\xi(\mathbf{M}) > 10^{10}$ (good value < 10)
- M is sparse
- M is big (memory problems)

$$\mathbf{y} = \mathbf{M}\mathbf{x} \longrightarrow \arg \min_{\mathbf{x}} \{f(\mathbf{x}, \mathbf{y}) + g(\mathbf{x})\}$$

Inverse Problem

- ill-posed problem $M \neq N$
- ill conditioned $\xi(\mathbf{M}) > 10^{10}$ (good value < 10)
- M is sparse
- M is big (memory problems)

$$\mathbf{y} = \mathbf{M}\mathbf{x} \longrightarrow \arg \min_{\mathbf{x}} \{f(\mathbf{x}, \mathbf{y}) + g(\mathbf{x})\}$$

Solvers:

- SART (well known)
- TVAL3 (complex to tune)

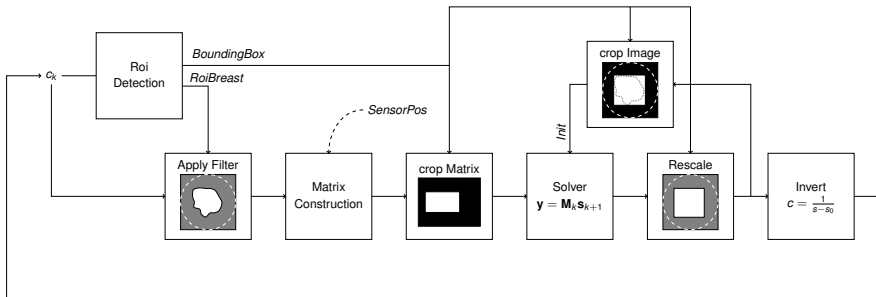
Our interest

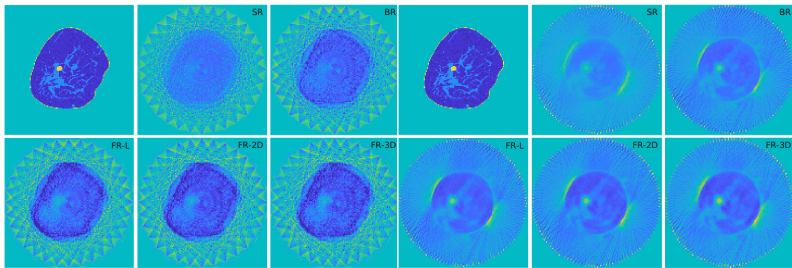
- Focus computation on the center of the aperture
- Faster
- Less background noise
- Memory efficient



Figure 10: Binary segmentation for ROI detection

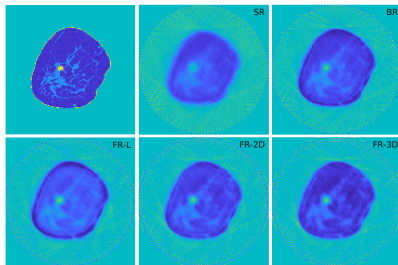
Reconstruction Procedure





(a) 32 transducers, 90° opening.

(b) 128 transducers, 30° opening.



(c) 128 transducers, 90° opening.

Figure 11: Opening and Number of Rays Influence

SART

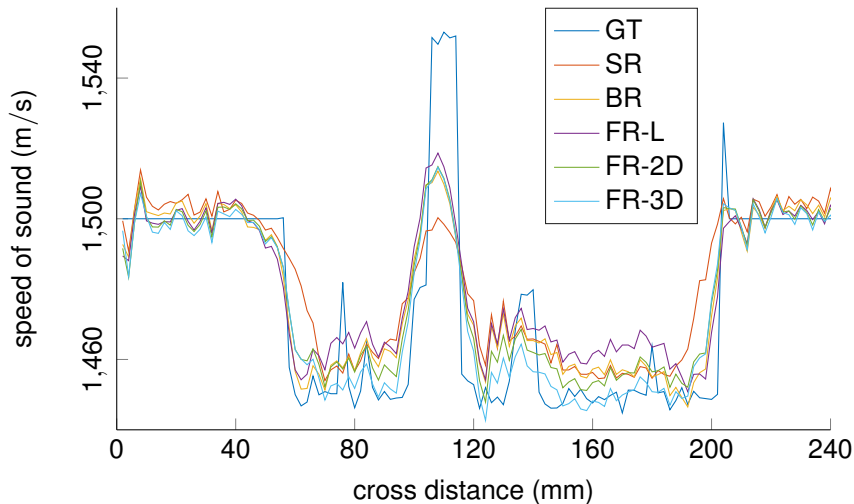


Figure 12: cross section of SART reconstruction ideal case

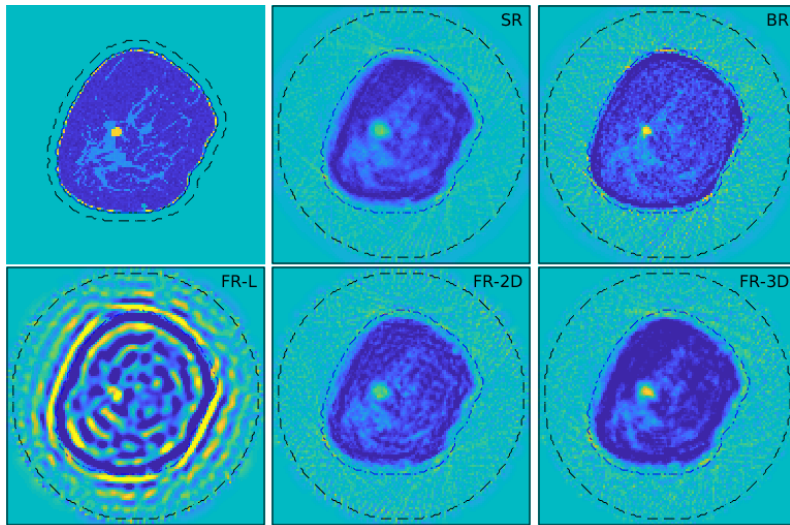


Figure 13: TVAL reconstruction, weak regularization on gradient ($\beta = 10^{-2}$, $\mu = 10^3$). 128 emitters, full opening angle.

TVAL Regularisation

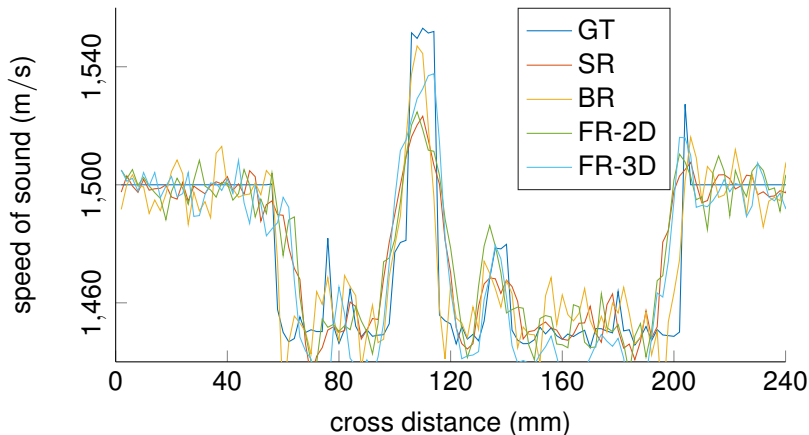
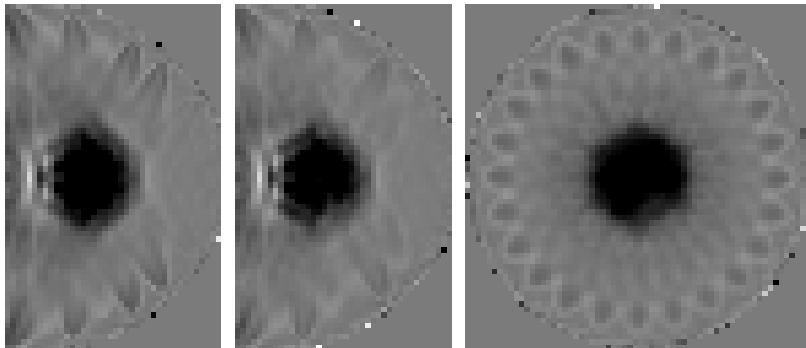
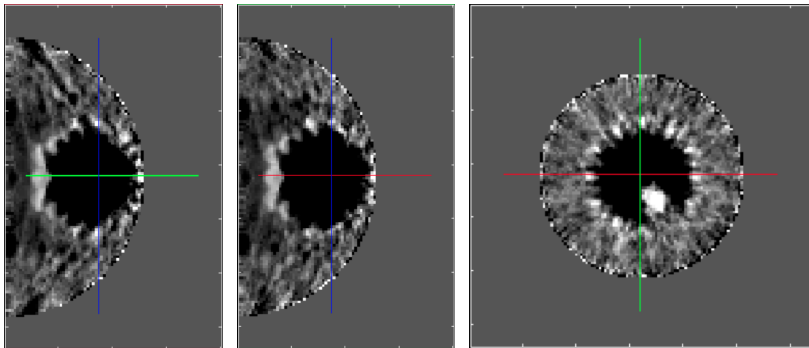


Figure 14: cross section of the TVAL reconstruction



3D phantom (64x64x50) reconstruction. 1 emitter for 4 receiver
Fat Ray Linear, SART, No TV, no ROI



3D phantom (64x64x50) reconstruction. 1 emitter for 4 receiver
Fat Ray, SART, Strong TV, ROI

Achievements

- Fat Ray implementation
- ROI-based computation
- 3D simulation and Regularisation
- SART more robust than TVAL

Future work ?

- C-MEX / GPU Implementation
- Experimental Data

Thank you for listening

any questions ?

Kernel expression

$$K_t^{3D}(\mathbf{y}) = \frac{s_0}{2\pi} \frac{\|\mathbf{x}_r - \mathbf{x}_e\|}{\|\mathbf{x}_r - \mathbf{y}\| \|\mathbf{y} - \mathbf{x}_e\|} \int_{\omega - \Delta\omega}^{\omega + \Delta\omega} A(\omega) \omega \sin(\omega s_0 \delta l(\mathbf{y})) d\omega$$

$$K_t^{2D}(\mathbf{y}) = \sqrt{\frac{s_0}{2\pi}} \sqrt{\frac{\|\mathbf{x}_r - \mathbf{x}_e\|}{\|\mathbf{x}_r - \mathbf{y}\| \|\mathbf{y} - \mathbf{x}_e\|}} \int_{\omega - \Delta\omega}^{\omega + \Delta\omega} A(\omega) \sqrt{\omega} \sin\left(\omega s_0 \delta l(\mathbf{y}) + \frac{\pi}{4}\right) d\omega$$

- Heavy computation
- Limits to Fresnel Zone
- No Hypothesis on slowness distribution
- Works also for attenuation

SART

$$\mathbf{x}^{(k+1)} = \mathbf{x}^{(k)} + \lambda \mathbf{C} \mathbf{M}^T \mathbf{R} (\mathbf{y} - \mathbf{M} \mathbf{x}^{(k)})$$

With \mathbf{C} and \mathbf{R} diagonal matrices use for the ponderation:

$$c_{jj} = \left(\sum_{i=1}^M |M_{i,j}| \right)^{-1} \quad r_{jj} = \left(\sum_{j=1}^N |M_{i,j}| \right)^{-1}$$

TVAL3

Solve with total variation Regularisation:

$$\min \|D_x \mathbf{x}\|_1 + \|D_y \mathbf{x}\|_1 + \|D_z \mathbf{x}\|_1 \text{ with } \mathbf{y} = \mathbf{M}\mathbf{x}$$

$$\mathcal{L}(\beta, \mu, \lambda, \nu) = \underbrace{\sum_i \left(\|w_i\| - \nu_i^T (D_i \mathbf{x} - w_i) + \frac{\beta}{2} \|D_i \mathbf{x} - w_i\|_2^2 \right)}_{\text{w-problem}} \quad (1)$$
$$\underbrace{- \lambda^T (\mathbf{M}\mathbf{x} - \mathbf{b}) + \frac{\mu}{2} \|\mathbf{M}\mathbf{x} - \mathbf{b}\|_2^2}_{\text{x-problem}}$$

- [1] HOPP, T., ZUCH, F., COMBY, P. A., et al. *Fat ray ultrasound transmission tomography: preliminary experimental results with simulated data.*
- [2] GEMMEKE H., HOPP T., ZAPF M., et al. *3D ultrasound computer tomography: Hardware setup, reconstruction methods and first clinical results.*
- [3] <https://perso.crans.org/comby/ipe/report.pdf>